

## 2d Solar Thermal Direct Absorption Comparison Between Gold And Silver Nanoparticle

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### ABSTRACT

In recent years, the application of nanoparticles for direct thermal absorption in solar energy technology has emerged as a transformative advancement, showing significant potential compared to traditional solar collectors. In this research, nanofluids containing silver and gold nanoparticles were simulated, using water and ethylene glycol as the base fluid. The simulations were carried out using a modelled rectangular test cell, employing constant heat flux conditions through the ANSYS Fluent software. This study builds upon prior research by extending the comprehension of how nanofluids, particularly those involving silver and gold nanoparticles, can enhance photothermal absorption rates. The primary objective of this paper is to conduct a comparative analysis of the photothermal absorption rates exhibited by the two nanofluids under two simulation cases: (1) a constant heat flux applied to only one side of the wall and (2) a constant heat flux applied to both sides of the wall. The results show that both silver and gold nanofluids have excellent photothermal absorption rate and increase significantly when heat flux is applied to both sides of the wall. A better performance is observed for silver ethylene glycol-based nanofluid. Therefore, for a more photothermal absorption rate, it is recommended that silver ethylene glycol based nanofluid should be used.

**Index-words:** Nanofluids, thermal absorption, solar collectors, photothermal absorption, gold nanofluid, silver nanofluid

### I. INTRODUCTION

Solar energy is a prominent renewable energy source that offers minimal environmental impact and has gained significant attention due to the increasing population and high electricity demand. It serves as a promising integral energy source, reducing greenhouse gas emissions and diversifying the energy supply [1]. With an annual solar energy production of  $1.74 \times 10^{17}$  W, it has the potential to meet global energy demands [2].

Solar energy can be captured through various methods, including photocatalytic, photoelectric, and photothermal conversion techniques [3]. In the realm of photothermal conversion, solar thermal collectors play a vital role in transforming solar energy into thermal energy, which can then be utilized for various applications. These collectors are broadly classified as concentrating and non-concentrating solar collectors, and further categorized as low, medium, and high temperature collectors [4].

To enhance the efficiency of solar thermal collectors, novel approaches have been explored, and nanofluids have emerged as a promising avenue. Nanofluids, which consist of nanoparticles suspended in a base fluid, have been extensively studied for their ability to improve

heat transfer in applications such as solar collectors, heat exchangers, and radiators [5], [6]. Nanofluids utilize nanoparticles with sizes less than 100 nm, offering better heat conduction than conventional fluids due to their molecular-level interaction with the base fluid [7].

The application of nanofluids in solar thermal collectors aims to achieve enhanced thermal properties, including higher thermal diffusivity, thermal conductivity, and convective heat transfer coefficient [7]. These properties are influenced by factors such as nanoparticle volume fraction, size, shape, and the choice of base fluid.

Several advantages of nanofluids have been identified, including strong surface Plasmon resonance, high specific surface area enabling efficient heat transfer, and high photothermal conversion properties. However, they also face limitations such as sedimentation and aggregation in the fluid, as well as higher production and preparation costs [5].

In the context of solar thermal applications, silver and gold nanoparticles have been extensively studied for their thermal properties. Table I presents the thermal properties of silver and gold nanoparticles [8]. Furthermore, the choice of base fluid, such as water and ethylene glycol, also influences the thermal properties,

as shown in Table II [9].

**TABLE I**  
**THERMAL PROPERTIES OF SILVER AND GOLD**  
**NANOPARTICLE [8], [10]**

Properties	Silver	Gold
Density (kg/m <sup>3</sup> )	10500	19300
Specific Heat (J/Kg. K)	230	129
Thermal Conductivity (W/mK)	429	314

**TABLE II**  
**THERMAL PROPERTIES OF WATER AND ETHYLENE**  
**GLYCOL BASE FLUID [9], [11]**

Properties	Water	Ethylene Glycol
Density (kg/m <sup>3</sup> )	997	863
Specific Heat (J/Kg. K)	4179	2048
Thermal Conductivity (W/mK)	0.613	0.1404

The simulation and experimental analysis of nanofluids within solar thermal collectors require suitable test cells. Acrylic glass, a transparent thermoplastic homopolymer, has been commonly used due to its impact resistance and optical clarity. It serves as a versatile and cost-effective alternative to traditional glass, making it ideal for experimental observations.

In this study, the efficiency of silver and gold nanoparticles as direct sunlight absorbers in solar thermal applications was investigated using water and ethylene glycol as base fluids. The performance of these nanofluids was simulated for both one-sided and double-sided heat flux cases to account for solar tracking. Additionally, a comparison between gold and silver nanoparticles and their respective base fluids was conducted. This paper seeks to:

1. Investigate the photo-thermal absorption rate of nanofluids: (a) Gold-water, (b) Gold-ethylene glycol, (c) silver-water, (D) silver-ethylene glycol, for both cases where heat flux is applied to one side of the wall and heat flux applied to both sides of the wall.
2. Compare the photothermal absorption rate of gold and silver nanofluids.

This study makes a substantial contribution to the ongoing progression of solar energy technology,

demonstrating the critical influence of nanofluid selection on photothermal absorption rates.

## II. LITERATURE REVIEW

Enhancing the performance of solar energy systems has been the subject of extensive research. One approach that has gained significant attention is the use of nanofluids as heat transfer fluids in solar collectors. Several studies have investigated the benefits of nanofluids in improving the efficiency of solar energy harvesting devices.

The study by Tyagi et al. [12] revealed that Direct Absorption Solar Collectors (DASCs) using nanofluids as the working fluid exhibited up to 10% higher efficiency compared to flat-plate collectors. The presence of nanoparticles (NPs) in the nanofluids increased solar energy absorption by more than nine times compared to pure water.

Concurrently, the study conducted by Chaji et al. [13] delved into the efficiency impact of TiO<sub>2</sub> nanoparticles, revealing efficiency enhancements of up to 15.7% with increased mass flow rates and up to 7% with TiO<sub>2</sub> particle additions.

Moreover, the thoughtful selection of nanofluids has emerged as a pivotal determinant in realizing performance increases within DASCs. For instance, Karami et al. [14] innovatively introduced carbon nanotube/water nanofluid into low-temperature DASCs, unveiling heightened photothermal conversion characteristics. Alongside, Meijie Chen et al. [15] conducted an exhaustive inquiry into the collector efficiency of silver nanofluids within direct absorption solar collectors, thus substantiating their prowess, particularly under real outdoor conditions.

Another valuable study by Ahmet Z. Sahin et al. [16] reiterated the efficiency gains achieved through nanofluid implementation. Their experiment yielded a notable 23.83% increase in solar collector efficiency compared to water. Intriguingly, they identified an optimum nanoparticle concentration, indicating the nonlinear nature of thermal conductivity's incremental trend.

A notable experimental investigation by Sanjay Kumar et al. [17] examined a direct absorption solar collector utilizing ultra-stable gold plasmonic nanofluid under real outdoor conditions. The outcomes of this study unveiled a remarkable enhancement in photothermal conversion efficiency, even at low particle loadings when gold nanoparticles (Au-NPs) were incorporated into water.

Parallel, Abdulhammed K. Hamzat et al. [18] conducted a comprehensive review that underscored the significance of nanofluid parameters on system performance. Their investigation indicated a 6.6% efficiency improvement

in a solar thermal system with CuO/water nanofluid compared to other conventional fluids. This aligns with related work by Menbari et al. [19], which demonstrated performance improvements in PTSC with CuO/water nanofluid and attributed the enhancement to nanofluid flow rate and nanoparticle volume fraction.

Similarly, the review by Panduro et al. [20] focused on the use of nanofluids as heat-transfer fluids in parabolic-trough collectors. It confirmed the well-established enhancement of thermal conductivity in nanofluids compared to base fluids. Various studies have investigated the dependence of thermal conductivity on nanofluid concentration and particle size.

**TABLE III**  
**SUMMARY OF RECENT RELATED WORKS**

Study	Key Findings
Tyagi et al. [12]	DASCs with nanofluids up to 10% more efficient than flat-plate collectors. Significant increase in solar energy absorption with NPs.
Chaji et al. [13]	TiO <sub>2</sub> nanoparticles led to efficiency increases of up to 15.7% with increased mass flow rates and up to 7% with particle additions.
Meijie Chen et al. [15]	Real outdoor conditions demonstrated efficiency enhancement of silver nanofluids in direct absorption solar collectors.
Ahmet Z. Sahin et al. [16]	Experimental efficiency gain of 23.83% with nanofluid; identification of an optimum nanoparticle concentration.
Sanjay Kumar et al. [17]	Ultra-stable gold plasmonic nanofluids showcased remarkable photothermal conversion efficiency even at low concentrations.
Abdulhammed K. Hamzat et al. [18]	Nanofluids' impact on efficiency across diverse solar energy applications; emphasis on optimizing parameters.

In conclusion, these reviewed studies collectively highlight the immense potential of nanofluids in enhancing the performance of solar energy harvesting devices. Nanofluids have demonstrated superior thermal conductivity, heightened solar energy absorption rates, and improved collector efficiency in contrast to conventional fluids. However, further research endeavors are warranted to fine-tune parameters such as nanoparticle concentration, volume fraction, and flow rates for the attainment of peak performance. The application of nanofluids in solar energy systems holds promise in addressing energy demands and mitigating

energy crises.

### III. METHODOLOGY

#### A. System Parameter

In this section, the governing equations and models are briefly explained.

##### 1. Transient flow

The simulation accounts for the transient nature of flow using the transient model in ANSYS. The solver solves each time step, eventually reaching a finite time step. Transient flows can be categorized into two types: forced transient and naturally occurring transients.

- **Forced Transient:** Time-dependent boundary conditions and source terms drive the transient flow field. Examples include rotor-stator interactions in a turbine or pulsing flow in a nozzle.
- **Naturally Occurring Transients:** Transient flow occurs due to the growth of instabilities within the fluid or a non-equilibrium initial fluid state. Examples include shock waves, heat absorption, and natural convection.

##### 2. Governing equations

These equations mathematically describe the behavior of fluids, allowing engineers and scientists to analyze and predict fluid flow patterns, velocities, pressures, and other important properties. The governing equations are derived from fundamental principles such as conservation of mass, momentum, and energy. There are three primary equations commonly used: the continuity equation, the Navier-Stokes equations, and the energy equation. The equations stem from the fundamental principles of Newton's Laws and Reynolds transport theorem.

#### Mass conservation equation:

Continuity equation can be written in its general form using Gauss' divergence theorem by B. Sultanian., [21] and Emanuel, G., [22] as:

$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho V) = S_m. \quad (1)$$

This equation is applicable to both compressible and incompressible flows. The source  $S_m$  is the mass added continuous phase from a second phase and other user defined sources. For 2D axisymmetric geometry, the mass conservation equation can be given as Emanuel, G., [22]:

$$\frac{\partial \rho}{\partial t} + \frac{\partial}{\partial x}(\rho v X) + \frac{\partial}{\partial r}(\rho v r) + \frac{\rho v r}{r} = S m. \tag{2}$$

Momentum Equation,

The Navier-Stokes equations, derived from Newton's second law of motion, describe the conservation of momentum in a fluid. The momentum equation in an inertial reference frame is given as:

$$\frac{\partial}{\partial t}(\rho \cdot v) + \nabla \cdot (\rho \vec{v} \vec{v}) = -\nabla P + \nabla \cdot (\bar{T}) + \rho \vec{g} + \vec{F}. \tag{3}$$

Where  $p$  being the static pressure,  $\bar{T}$  is the stress tensor, and  $\vec{g}$  and  $\vec{F}$  are the gravitational force and external body forces.

The stress tensor is given by:

$$\bar{T} = \mu[(\nabla \vec{v} + \nabla \vec{v}^T) - \frac{2}{3} \nabla \cdot \vec{v} I] \tag{4}$$

Where  $\mu$  is the molecular viscosity,  $I$  is the unit tensor and the second term on the right-hand side is the effect of volume dilation. Special practices related to the discretization of the momentum and continuity equation and their solution by means of the pressure-based solver are addressed in Ansys, (2009)

### 3. Multi-phase flow

Real-life flows often involve multiple phases. In multi-phase flow, a phase is defined as an identifiable class of material that has a particular inertial response to and interaction with the flow and potential field. The simulation considers multiple phases, such as liquid, gas, and solid (Ansys, 2012)

### 4. Volume of fraction (VOF)

The Volume of Fraction (VOF) model is a surface-tracking technique applied to a fixed Eulerian mesh. It is used for two or more immiscible fluids where the position of the interface between the fluids is of interest. The VOF model shares a single set of momentum equations for the fluids and tracks the volume fraction of each fluid in each computational cell throughout the domain (Ansys, 2010).

### 5. Modelling of nanofluid properties

It is important to determine the properties of nanofluid when solving the conservation equations. The needed properties include specific heat capacity, thermal conductivity, density, and dynamic viscosity. Using the following equations, the properties of gold and silver nanofluid were accounted for.

$$\rho_{nf} = \phi \rho_{np} + (1 - \phi) \rho_{bf} \tag{5}$$

The density of nanofluids is based on the mixture rule by Liu et al [23]

$$\mu_{nf} = (1 + 2.5\phi) \mu_{bf} \tag{6}$$

The viscosity is calculated considering the Brownian motion used by Batchelor et al. [24]

$$c_{p,nf} = \phi c_{p,np} + (1 - \phi) c_{p,bf} \tag{7}$$

This specific heat is calculated based on the theoretical model by Gupta et al. [25]

$$k_{nf} = k_{bf} + \left( \left[ 1 + \frac{3(k_{np} - k_{bf})\phi}{k_{nf} + 2k_{bf} - (k_{np} - k_{bf})\phi} \right] \right) \tag{8}$$

This thermal conductivity of nanofluid is calculated using the theoretical model of Xuan et al. [26]

### B. Geometry and Mesh

Using Ansys® Space claim a 2D geometry that represented the setup was designed, with all the necessary constraints needed for solving a boundary value problem.

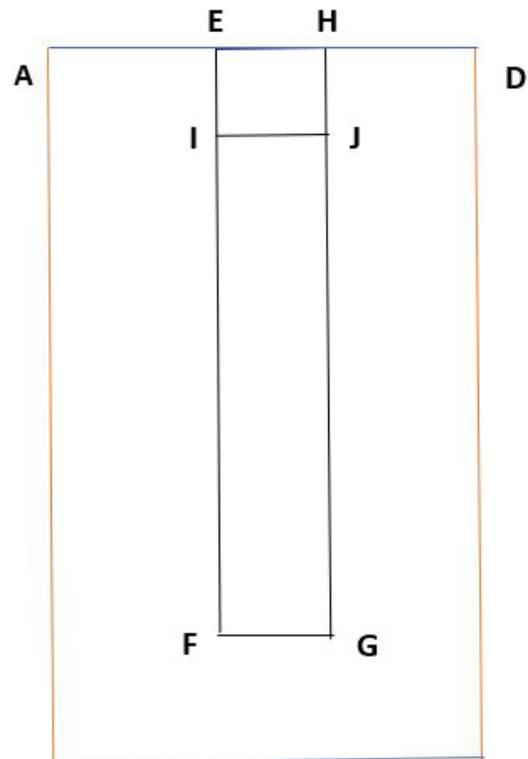


Fig. 1. Geometry

The walls AB and DC are exposed to sunlight (Heat flux is applied). While the wall EH is the pressure outlet, the remaining walls are all adiabatic. The geometry is then meshed to break the larger domain into pieces, which represents elements that can be designed in terms of the physical shape of the domain.

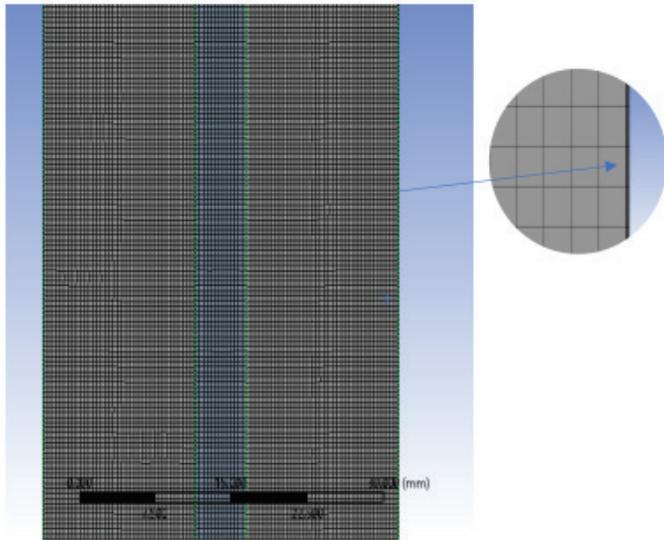


Fig.2. Mesh and inflation layers

Meshing is done to help reduce computational time and improve accuracy. During the meshing process five inflation layers were placed in the walls that have heat flux applied to them and the walls of the nanofluid region, to help capture the temperature profiles correctly near the no slip walls. A grid independence test was performed to find the optimal grid size for the simulation.

**C. Simulation Setup**

The simulation is carried out in Ansys® Fluent where the following parameters were setup.

TABLE IV  
 SIMULATION PARAMETERS

Solver	Pressure Based
Time	Transient
Total Time	7200 seconds
Step time	1
Materials	Nanofluid/Acrylic glass
Phase	Multi-phase
Scheme	Piso
Gradient	Least Square Cell Based
Formulation	Second Order Implicit
Initialization	Hybrid

The simulation was done in two cases where the heat flux is applied to just one side of the wall and the other case where the heat flux is applied to both sides of the walls. The Heat flux was calculated based on the geo-location with the help of the NASA and Solar Energy Database. To take into account the temperature profiles, surface monitors were placed on different points of the

surface. This would help capture the temperature at different time steps as the simulation goes on.

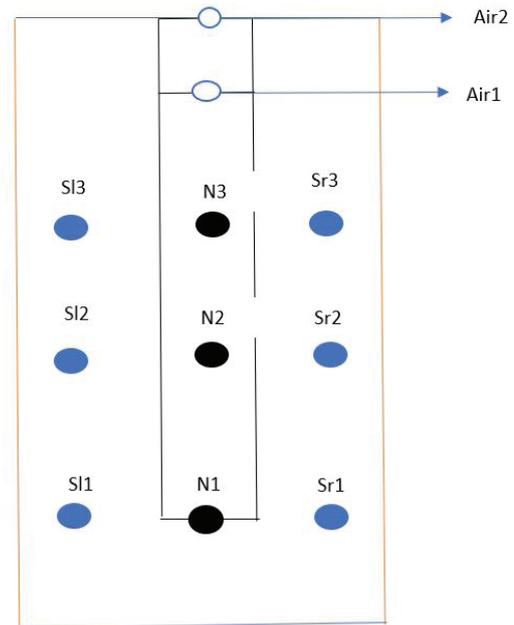
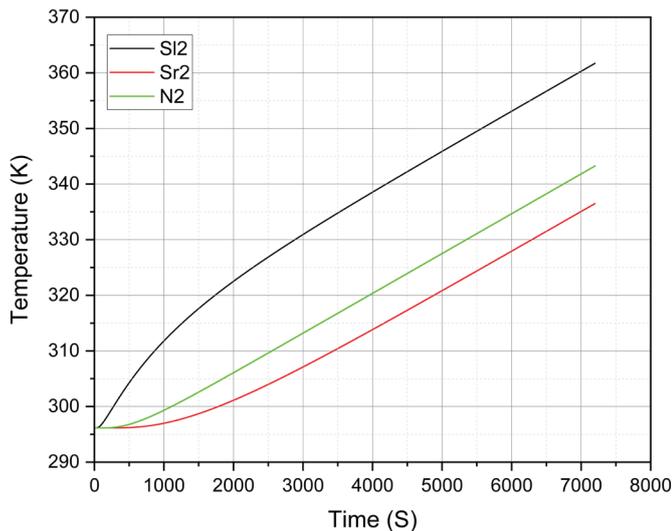


Fig.3. Surface monitors at different positions

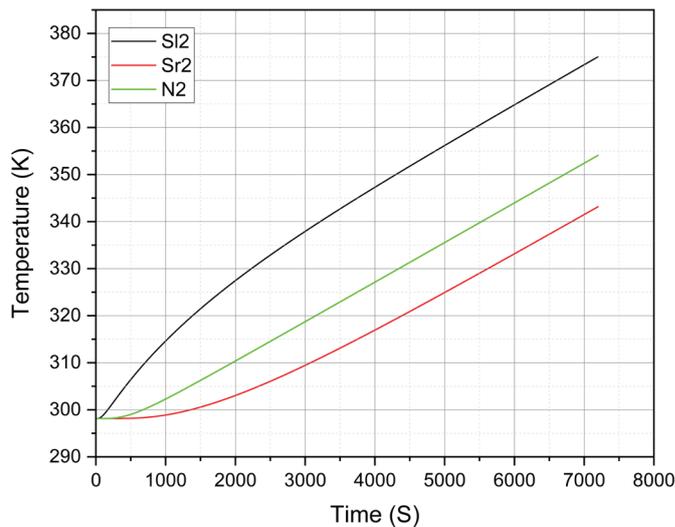
Six surface monitors are placed in the acrylic glass region, three in the nanofluid region and two in the air region. The simulation focused on the SI2, Sr2 and N2 surface monitors.

**IV. Simulation Results**

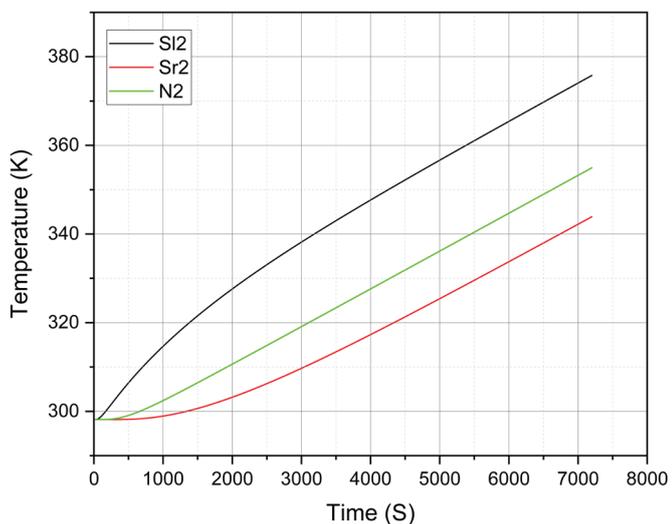
One of the difficulties faced in the simulation was how to factor in solar tracking. Since the simulation was 2D, the solar loading model could not be used, rather two cases were simulated, the first case is where the heat flux was applied to only one side of the wall to represent the solar irradiation at that side only, and the second case was simulated with the heat flux applied to both sides of the wall. Pressure was also neglected since the simulation involved a stationary nanofluid with no significant fluid motion. This analysis focuses on a two-hour period, a choice necessitated by constraints in computational resources, comparing different types of nanoparticles and base fluids under similar conditions. Temperature profiles for the simulation in the first case, where heat flux is only applied to the left side of the wall, are shown in Figures 4, 5, 6, and 7. The initial temperature for the simulation was 298.15 K.



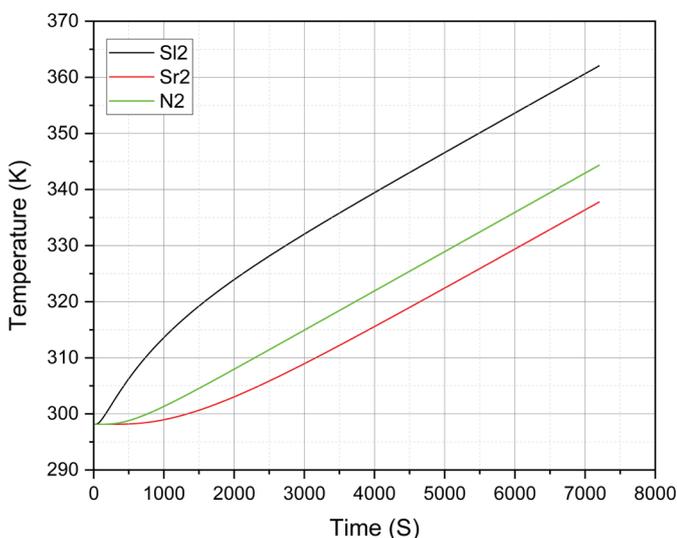
**Fig.4. Temperature profile of Ag water-based nanofluid**



**Fig.7. Temperature profile of Au ethylene glycol-based nanofluid**



**Fig.5. Temperature profile of Ag ethylene glycol-based nanofluid**



**Fig.6. Temperature profile of Au water-based nanofluid**

In the first case, where heat flux was applied to only one side of the wall, several intriguing observations were made. The temperature profiles revealed distinct temperature variations across different regions. The side of the wall with the heat flux (SI2) exhibited the highest temperature, followed by the nanofluid region (N2), while the other wall without heat flux had the lowest temperature. These results highlight the impact of localized heat application and the subsequent thermal distribution within the system. However, it is important to note that the temperature variations were not uniform and were influenced by the specific nanoparticle and base fluid combinations used in the simulations. Analyzing the temperature profiles for different nanofluids, showed remarkable differences based on the choice of base fluid. For instance, in Figure 4, the temperature within the nanofluid region (N2) increased from an initial 298.15 K to 343.3 K, while the temperature within the left acrylic wall (SI2) rose from 298.15 K to 361.7 K. In Figure 5, a similar trend is observed, with the temperature of the N2 region increasing from 298.15 K to 354.95 K and SI2 reaching 375.78 K. These findings indicate a notable temperature increase of 19% and 26% in the nanofluid (N2) and left acrylic wall region (SI2), respectively, when using an ethylene glycol base fluid. For water as the base fluid, the temperature increased by 15% in N2 and 21% in SI2.

Figures 6 and 7 show a similar temperature pattern, with the N2 region reaching 344.33 K and 354.1 K, respectively, while SI2 reached 362.05 K and 375.05 K. Using a water base fluid with gold nanoparticles (Au), a temperature increase of 15.5% in N2 and 21.4% in SI2 was recorded. When employing ethylene glycol as the base fluid, the temperature increased by 18.8% in N2 and 25.8% in SI2 respectively.

In the second case of the simulation, heat flux was applied to both sides of the wall. The temperature profile for the second case is shown in Figures 8, 9, 10 and 11.

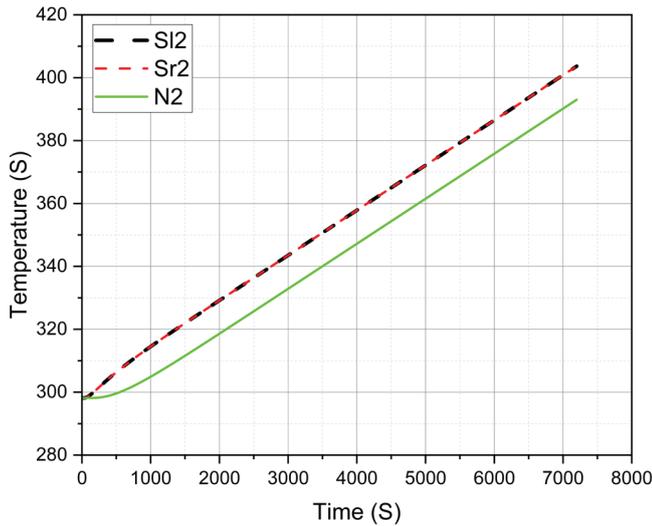


Fig. 8. Temperature profile of Ag water-based nanofluid

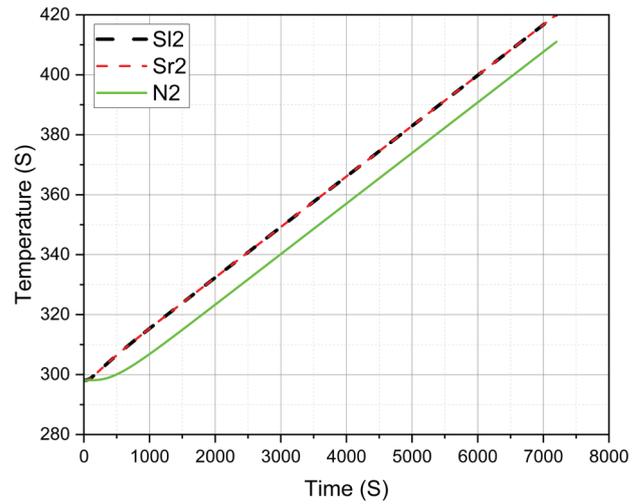


Fig.11. Temperature profile of Au ethylene glycol-based nanofluid

In a distinct set of experiments, the effects of uniform heat flux application to both the left acrylic wall region (SI2) and the right acrylic wall region (Sr2) were examined. Consequently, SI2 and Sr2 exhibited similar temperature profiles due to the uniform distribution of heat flux on both sides of the wall.

However, it is crucial to highlight that these temperature variations were non-uniform within the nanofluids themselves, as evident in Figures 8 and 9. In Figure 8, the temperature within the Nanofluid region (N2) increased substantially from 298.15 K to 393.04 K, while both SI2 and Sr2 regions experienced an increase from 298.15 K to 403.67 K. Figure 9 followed a similar pattern, with the temperature profile of N2 rising from 298.15 K to 412.74 K and SI2 and Sr2 temperatures rising from 298.15 K to 421.54 K.

These experiments utilized silver nanoparticles (Ag) within the nanofluid, with the choice of base fluid once again serving as the distinguishing factor. When employing water as the base fluid, the observed temperature gains were 31.83% in the nanofluid region (N2) and 35.39% in both acrylic wall regions (SI2 and Sr2). Conversely, when ethylene glycol was employed as the base fluid, the recorded temperature enhancements were 38.43% in N2 and 41.39% in the acrylic wall regions (SI2 and Sr2), respectively.

Finally, a consistent trend was observed in Figures 10 and 11, affirming the influence of base fluid choice on temperature profiles. In Figure 10, the temperature within N2 increased by 31.05%, and within SI2 and Sr2, there was a temperature increase of 34.72%, all while using water as the base fluid. In Figure 11, employing ethylene glycol as the base fluid, a similar pattern emerged, with a 37.86% temperature increase in N2 and a 40.9% temperature increase in both acrylic wall

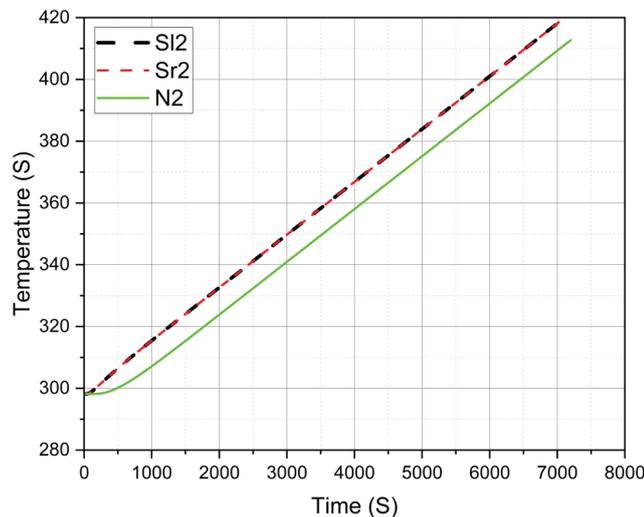


Fig. 9. Temperature profile of Ag ethylene glycol-based nanofluid

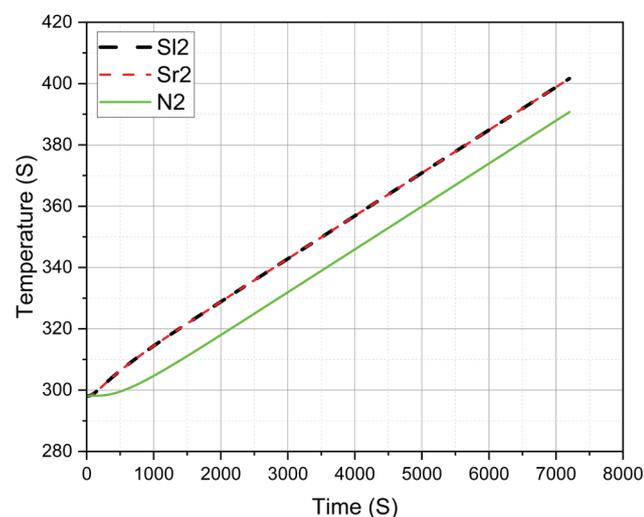


Fig.10. Temperature profile of Au water-based nanofluid

regions (Sl2 and Sr2).

These extensive experiments underline the importance of base fluid selection within nanofluid systems, which can significantly impact temperature profiles and, consequently, the overall performance of heat transfer applications.

## V. DISCUSSION

These findings demonstrate the significant influence of the base fluid on heat transfer characteristics and emphasize the importance of considering the thermophysical properties of the fluid when designing heat transfer systems. Tyagi et al. [12] highlight the importance of selecting the right nanofluid in improving the efficiency of solar energy harvesting devices. The results obtained from this simulation suggests that using ethylene glycol as a based fluid would provide higher thermal absorption as compared to water.

Similar trends were observed for gold nanofluids, indicating that the choice of base fluid remains a crucial factor in determining the system's thermal behavior. The temperature variations across different regions were consistent with those observed in the silver nanofluid simulations. These results suggest that the enhanced thermal performance attributed to nanoparticles is further influenced by the specific properties of the base fluid.

In the second case, where heat flux was applied to both sides of the wall, an entirely different temperature distribution pattern emerged. In this case, both sides of the wall experienced the highest temperatures. The equal application of heat flux on each side resulted in similar temperature rises, as expected. Comparing these results with those of the first case, it is evident that the temperature increases were more pronounced when heat flux was applied to both sides. This finding highlights the synergistic effect of dual-sided heat application, which leads to enhanced thermal characteristics within the system.

Upon examining the effects of different base fluids in the second case, it is observed that the choice of base fluid continued to play a pivotal role. When water was employed, silver nanofluid exhibited a 32% increase in temperature for N2 and a 35% increase for both walls (Sl2/Sr2). On the other hand, using ethylene glycol as the base fluid, the temperature increased by 38% in N2 and 41% in both walls. These results emphasize the significance of the base fluid in achieving optimal thermal performance and demonstrate the potential for further enhancing heat transfer efficiency in systems utilizing nanofluids. The results obtained are in line with Kumar et al. [17] investigation on ultra-stable gold plasmonic nanofluid. Both studies observed an increased efficiency

of the working fluid. A comparison of the temperature changes in the nanofluids is presented in Table V.

**TABLE V**  
**TEMPRETURE AT NANOFLUID REGION (N2)**

Cases	Nanofluid Region (N2) Temperature (K)				
	Nano particles Base fluids	Gold		Silver	
		water	ethylene glycol	water	ethylene glycol
1	Initial	298.15	298.15	298.15	298.15
	Final	344.33	353.1	343.26	354.95
	Temperature ( $\Delta T$ )	<b>15.49%</b>	<b>18.43%</b>	<b>15.13%</b>	<b>19.05%</b>
2	Initial	298.15	298.15	298.15	298.15
	Final	390.73	411.04	393.035	412.74
	Temperature ( $\Delta T$ )	<b>31.05%</b>	<b>37.86%</b>	<b>31.83%</b>	<b>38.43%</b>

Comparing the performance of silver and gold nanofluids, it becomes evident that both types contribute significantly to an improved heat transfer coefficient, particularly when heat flux is applied to both walls. Furthermore, these findings highlight the superior thermal performance achieved by selecting ethylene glycol as the base fluid over water. This underscores the critical importance of meticulously considering the thermophysical properties of the base fluid during the design phase of heat transfer systems, an assertion made by Hamzat et al. [18] who similarly observed an increase in the thermal efficiency of solar thermal systems employing CuO/water nanofluids. These results are in alignment with the investigative experiment conducted by Filho et al. [27], which demonstrated a substantial increase in the thermal energy of silver nanofluids.

Additionally, comparing the silver ethylene glycol-based nanofluid with the gold ethylene glycol-based nanofluid, a 1% higher thermal absorption rate was observed in the silver nanofluid. While this difference may appear negligible in the short term, it holds importance for long-term simulations and should be considered when running simulations over extended periods.

This study introduces a critical factor that has been relatively less explored in previous research: the pivotal role of base fluid selection, especially when confronted with dual-sided heat application cases. The findings vividly illustrate how the choice of base fluid can exert substantial influence over temperature profiles and overall thermal performance. A remarkable temperature increases is observed achievable through the astute selection of base fluids, underscoring the potential for further optimization of heat transfer efficiency in nanofluid-based systems. In doing so, the study expands

the scope of knowledge in the field and contributes essential insights into the effective utilization of nanofluid for enhanced energy harvesting and heat transfer processes.

## VI. CONCLUSION

The study investigated the effects of nanoparticle type and base fluid selection on the temperature profiles and heat transfer characteristics of nanofluids through a 2D simulation. Silver and Gold nanoparticles with water and ethylene glycol base fluids were investigated to study their photothermal absorption rate. The findings of this study underscore the critical role played by the choice of base fluid in nanofluid-based heat transfer systems. Notably, it was observed that the application of heat flux to both sides of the wall, as opposed to a single side, resulted in a significant increase in the photothermal absorption rate. This emphasizes the importance of solar tracking mechanisms to maximize photothermal efficiency, considering the dynamic positioning of the Earth relative to the sun. The results suggest that the use of ethylene glycol as base fluid in nanofluids should be used more often rather than water. The use of gold and silver nanofluid are promising since they both are good plasmonic materials and have good thermal conductivity but the enhancement of photothermal absorption is better found in silver nanofluid using ethylene glycol as its base fluid.

Nanofluids offer potential gains in energy efficiency, cost savings, and reduced greenhouse gas emissions, supporting sustainability. Enhanced thermal performance through nanofluids could lead to downsizing heat system components and wider adoption of renewable energy, fostering long-term economic benefits and energy security.

Further research is essential to comprehensively comprehend the complex dynamics and long-term performance of nanofluids in solar harvesting devices, encompassing considerations like nanoparticle stability, simulation time, system component effects, cost-effectiveness, and scalability.

## VII. References

- [1] C. Voyant *et al.*, "Machine learning methods for solar radiation forecasting: A review," *Renewable Energy*, vol. 105, 2017. doi: 10.1016/j.renene.2016.12.095.
- [2] P. Kumari, and T. Durga, "Deep learning models for solar irradiance forecasting: A comprehensive review." *Journal of Cleaner Production* 318 (2021): 128566.
- [3] A. R. Mallah, M. N. Mohd Zubir, O. A. Alawi, K. M. Salim Newaz, and A. B. Mohamad Badry, "Plasmonic nanofluids for high photothermal conversion efficiency in direct absorption solar collectors: Fundamentals and applications," *Solar Energy Materials and Solar Cells*, vol. 201, 2019, doi: 10.1016/j.solmat.2019.110084.
- [4] J. Hanania, K. Stenhouse., Brodie Yyelland, J. Don- ev. Solar Collector. 2018; Available from: [https://energyeducation.ca/encyclopedia/Solar\\_collector](https://energyeducation.ca/encyclopedia/Solar_collector).
- [5] K. Farhana *et al.*, "Improvement in the performance of solar collectors with nanofluids – A state-of-the-art review," *Nano-Structures and Nano-Objects*, vol. 18, 2019. doi: 10.1016/j.nano- so.2019.100276.
- [6] I. H. Yilmaz and A. Mwesigye, "Modeling, simulation and performance analysis of parabolic trough solar collectors: A comprehensive review," *Applied Energy*, vol. 225, 2018. doi: 10.1016/j.apener- gy.2018.05.014.
- [7] Ahmed, Mahmoud Salem. "Nanofluid: new fluids by nanotechnology." In *Thermophysical properties of Complex materials*. London, UK: IntechOpen, 2019.
- [8] M. Nazeer, K. Ramesh, H. Farooq, and Q. Shahzad, "Impact of gold and silver nanoparticles in highly viscous flows with different body forces," *International Journal of Modelling and Simulation*, 2022, doi: 10.1080/02286203.2022.2084217.
- [9] P. K. Pattnaik, J. R. Pattnaik, S. R. Mishra, and K. S. Nisar, "Variation of the shape of Fe<sub>3</sub>O<sub>4</sub>-nanoparticles on the heat transfer phenomenon with the inclusion of thermal radiation" *Journal of Thermal Analysis and Calorimetry*, vol. 147, no. 3, 20218, doi: 10.1007/s10973-021-10605-9.
- [10] S. Aghakhani, M. Afrand, A. Karimipour, R. Kalbasi, and M. Mehdi Razzaghi, "Numerical study of the cooling effect of a PVT on its thermal and electrical efficiency using a Cu tube of different diameters and lengths," *Sustainable Energy Technologies and Assessments*, vol. 52, 2022, doi: 10.1016/j.seta.2022.102044.
- [11] H. F. Oztop, A. Z. Sahin, H. Coşanay, and I. H. Sahin, "Three-dimensional computational analysis of performance improvement in a novel designed solar photovoltaic/thermal system by using hybrid nanofluids," *Renew Energy*, vol. 210, 2023, doi: 10.1016/j.renene.2023.04.115.
- [12] H. Tyagi, P. Phelan, and R. Prasher, "Predicted efficiency of a Low-temperature Nanofluid-based direct absorption solar collector," *Journal of Solar Energy Engineering, Transactions of the ASME*, vol. 131, no. 4, 2009, doi: 10.1115/1.3197562.
- [13] H. Chaji, Y. Ajabshirchi, E. Esmaeilzadeh, S. Z. Heris, M. Hedayatizadeh, and M. Kahani, "Experimental study on thermal efficiency of flat plate solar collector using tio<sub>2</sub>/water nanofluid," *Mod Appl Sci*, vol. 7, no. 10, 2013, doi: 10.5539/mas.v7n10p60.
- [14] M. Karami, M. A. Akhavan Bahabadi, S. Delfani,

- and A. Ghozatloo, "A new application of carbon nanotubes nanofluid as working fluid of low-temperature direct absorption solar collector," *Solar Energy Materials and Solar Cells*, vol. 121, 2014, doi: 10.1016/j.solmat.2013.11.004.
- [15] M. Chen, Y. He, J. Zhu, and D. Wen, "Investigating the collector efficiency of silver nanofluids based direct absorption solar collectors," *Appl Energy*, vol. 181, 2016, doi: 10.1016/j.apenergy.2016.08.054.
- [16] A. Z. Sahin, M. A. Uddin, B. S. Yilbas, and A. Al-Sharafi, "Performance enhancement of solar energy systems using nanofluids: An updated review," *Renew Energy*, vol. 145, 2020, doi: 10.1016/j.renene.2019.06.108.
- [17] S. Kumar, V. Sharma, M. R. Samantaray, and N. Chander, "Experimental investigation of a direct absorption solar collector using ultra stable gold plasmonic nanofluid under real outdoor conditions," *Renew Energy*, vol. 162, 2020, doi: 10.1016/j.renene.2020.10.017.
- [18] A. K. Hamzat, M. I. Omisanya, A. Z. Sahin, O. Ropo Oyetunji, and N. Abolade Olaitan, "Application of nanofluid in solar energy harvesting devices: A comprehensive review," *Energy Conversion and Management*, vol. 266, 2022. doi: 10.1016/j.enconman.2022.115790.
- [19] A. Menbari, A. A. Alemrajabi, A. Rezaei, "Heat transfer analysis and the effect of CuO/Water nanofluid on direct absorption concentrating solar collector", *Applied Thermal Engineering*, Volume 104, 2016, doi: 10.1016/j.applthermaleng.2016.05.064.
- [20] E. A. Chavez Panduro, F. Finotti, G. Largiller, and K. Y. Lervåg, "A review of the use of nanofluids as heat-transfer fluids in parabolic-trough collectors," *Applied Thermal Engineering*, vol. 211, 2022. doi: 10.1016/j.applthermaleng.2022.118346.
- [21] Sultanian, B. (2015). *Fluid Mechanics: An Intermediate Approach* (1st ed.). CRC Press. <https://doi.org/10.1201/b18762>
- [22] Emanuel, G. (2016). *Analytical Fluid Dynamics* (3rd ed.). CRC Press. <https://doi.org/10.1201/9781315148076>
- [23] J. Liu *et al.*, "Fullerene pipes," *Science* (1979), vol. 280, no. 5367, 1998, doi: 10.1126/science.280.5367.1253.
- [24] G. K. Batchelor, "The effect of Brownian motion on the bulk stress in a suspension of spherical particles," *J Fluid Mech*, vol. 83, no. 1, 1977, doi: 10.1017/S0022112077001062.
- [25] H. K. Gupta, G. Das Agrawal, and J. Mathur, "An experimental investigation of a low temperature Al<sub>2</sub>O<sub>3</sub>-H<sub>2</sub>O nanofluid based direct absorption solar collector," *Solar Energy*, vol. 118, 2015, doi: 10.1016/j.solener.2015.04.041.
- [26] Y. Xuan, Q. Li, W. Hu, "Aggregation structure and thermal conductivity of nanofluids," *AIChE J.* 49 (2003)
- [27] E. P. B. Filho, O. S. H. Mendoza, C. L. L. Beicker, A. Menezes and D. Wen, "Experimental investigation of a silver nanoparticle-based direct absorption solar thermal system." *Energy conversion and Management* 84 (2014): 261-267, ISSN 0196-8904.